

ASME DETC 2010

**A Second-Order Reliability Method  
with First-Order Efficiency**

**Xiaoping Du**

Missouri S&T

**Junfu Zhang**

Xihua University

# Outline

- Objective
- Background
- Methodology
- Examples
- Conclusions

# Objective

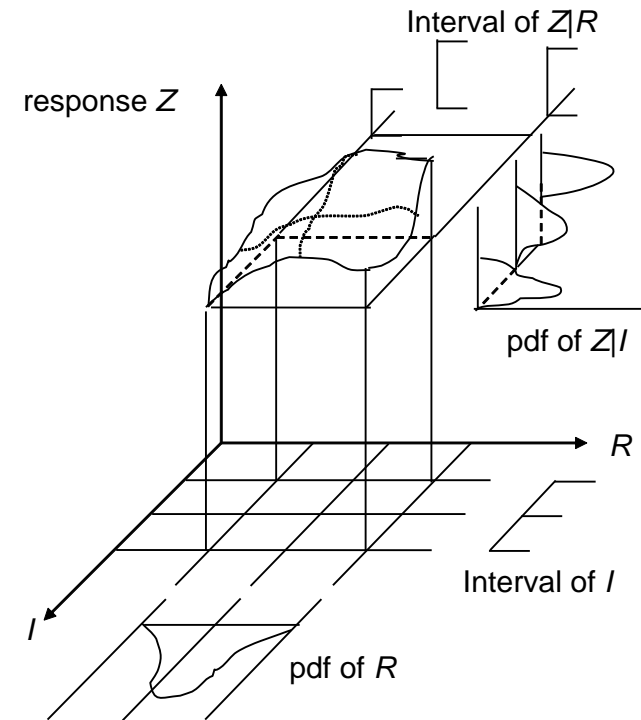
- Improve the efficiency of the FORM (First Order Reliability Method)
- Preserve the efficiency of the FORM
- Avoid sampling-based method

# Background - FORM

# Robustness with R and I

- Robustness measured by standard deviation (std) of  $Z$ ,  $\sigma_Z$
- Because of **I**,

$$\sigma_Z^{\min} \leq \sigma_Z \leq \sigma_Z^{\max}$$



# Task

- Given
    - Distributions of **R**
    - Width of **I**
  - Find
    - Effect of **R**: average std
- Effect of **I**, std difference

$$\bar{\sigma}_Z = \frac{1}{2} (\sigma_Z^{\max} + \sigma_Z^{\min})$$

$$\delta\sigma_Z = \sigma_Z^{\max} - \sigma_Z^{\min}$$

# Challenges

- $Z = f(\mathbf{X}) = f(\mathbf{R}, \mathbf{I})$ 
  - $f$  is nonlinear and expensive
  - Large dimension of  $(\mathbf{R}, \mathbf{I})$
  - Probabilistic analysis (PA) for  $\sigma_Z$
  - Interval analysis (IA) for  $\sigma_Z^{\max}$  and  $\sigma_Z^{\min}$
- Solution: Taylor expansion

# Problem with the 1<sup>st</sup> Order Expansion

- $Z = f(\mathbf{R}, \mathbf{I})$

$$\Delta Z = f(\mathbf{R}, \mathbf{I}) - f(\bar{\mathbf{R}}, \bar{\mathbf{I}}) \approx \sum_{i=1}^{nR} \left. \frac{\partial f}{\partial R_i} \right|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} \Delta R_i + \sum_{j=1}^{nI} \left. \frac{\partial f}{\partial I_j} \right|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} \Delta I_j = \nabla_{\mathbf{R}}^T \Delta \mathbf{R} + \nabla_{\mathbf{I}}^T \Delta \mathbf{I}$$

- Assume  $R_i$  are independent

$$\sigma_z = \sqrt{(\nabla_{\mathbf{R}}^T)^2 \sigma_{\mathbf{R}}^2} = \sqrt{\sum_{i=1}^{nR} \left( \left. \frac{\partial g}{\partial R_i} \right|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} \right)^2} \sigma_{R_i}$$

- **Problem:** no  $\sigma_Z^{\min}$  and  $\sigma_Z^{\max}$



# Semi-2<sup>nd</sup>-Order Approximation

$$\Delta f(\mathbf{R}, \mathbf{I}) = \nabla_{\mathbf{R}}^T \Delta \mathbf{R} + \nabla_{\mathbf{I}}^T \Delta \mathbf{I} + \frac{1}{2} \Delta \mathbf{X}^T \nabla^2 \Delta \mathbf{X}$$

Interaction terms of  
**R** and **I** are kept.

$$\nabla^2 = \begin{pmatrix} & & & \frac{\partial^2 g}{\partial R_1 \partial I_1} & \dots & \frac{\partial^2 g}{\partial R_1 \partial I_{nI}} \\ & & 0 & \dots & \dots & \dots \\ & & & \frac{\partial^2 g}{\partial R_{nR} \partial I_1} & \dots & \frac{\partial^2 g}{\partial R_{nR} \partial I_{nI}} \\ \frac{\partial^2 g}{\partial R_1 \partial I_1} & \dots & \frac{\partial^2 g}{\partial R_1 \partial I_{nI}} & & & \\ \dots & \dots & \dots & & & 0 \\ \frac{\partial^2 g}{\partial R_{nR} \partial I_1} & \dots & \frac{\partial^2 g}{\partial R_{nR} \partial I_{nI}} & & & \end{pmatrix}$$

# $\sigma_z$ Bounds

$$\sigma_z = \sqrt{\sum_{i=1}^{nR} \left( \frac{\partial f}{\partial R_i} \Big|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} + \sum_{j=1}^{nI} \frac{\partial^2 f}{\partial R_i \partial I_j} \Big|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} \Delta I_j \right)^2} \sigma_{Ri}^2$$

Calls  $f$  function  $(nR + 3 \times nR \times nI + 1)$  times

For  $\sigma_z^{\min}$

$$\min_{\mathbf{I}} \sum_{i=1}^{nR} \left( \frac{\partial f}{\partial R_i} \Big|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} + \sum_{m=1}^{nI} \frac{\partial^2 f}{\partial R_i \partial I_j} \Big|_{\bar{\mathbf{R}}, \bar{\mathbf{I}}} \Delta I_j \right)^2 \sigma_i^2$$

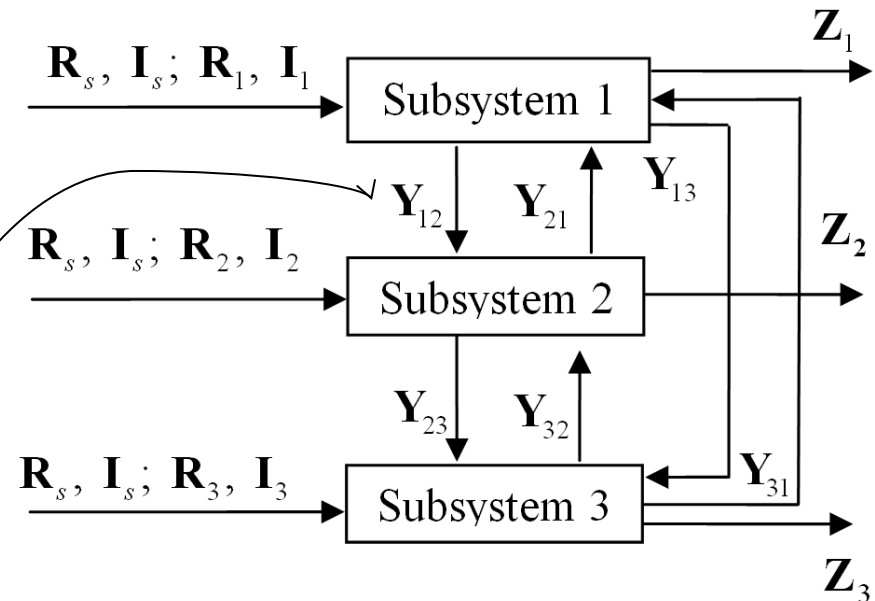
*s.t.*  $\mathbf{I}^l \leq \mathbf{I} \leq \mathbf{I}^u$

No  $f$  function calls

# Multidisciplinary Systems

Multidisciplinary analysis  
(MDA)

- Given:  $\mathbf{R}, \mathbf{I}$
- Find:  $\mathbf{Z}$
- Step 1: solve  $\mathbf{Y}$ 
  - $\mathbf{Y}_{ij} = \mathbf{Y}_{ij}(\mathbf{R}_s, \mathbf{I}_s, \mathbf{R}_i, \mathbf{I}_i, \mathbf{Y}_{.i})$
- Iterative process
- Step 2: solve  $\mathbf{Z}_i$ 
  - $\mathbf{Z}_i = \mathbf{Z}_i(\mathbf{R}_s, \mathbf{I}_s, \mathbf{R}_i, \mathbf{I}_i, \mathbf{Y}_{.i})$



Linking variables

Robustness assessment  
needs to call MDA repeatedly.



# Robustness Assessment

- Step 2 – Solve  $Z_i$ 
  - Semi-2<sup>nd</sup>-Taylor expansion

$$\Delta \mathbf{Z}_i = \mathbf{A}_i^Z \Delta \mathbf{R}_s + \mathbf{B}_i^Z \Delta \mathbf{R}_i + \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_i} \Delta \mathbf{Y}_i + \mathbf{M}_i^Z (\mathbf{I}_s, \mathbf{I}_i)$$

$$\mathbf{A}_i^Z = \begin{pmatrix} \frac{\partial Z_{i,1}}{\partial R_{s,1}} + \sum_{k=1}^{nS_I} \frac{\partial^2 Z_{i,1}}{\partial R_{s,1} \partial I_{s,k}} & \dots & \frac{\partial Z_{i,1}}{\partial R_{s,nSR}} + \sum_{k=1}^{nS_I} \frac{\partial^2 Z_{i,1}}{\partial R_{s,nSR} \partial I_{s,k}} \\ \dots & \dots & \dots \\ \frac{\partial Z_{i,n_{ij}}}{\partial R_{s,1}} + \sum_{k=1}^{nS_I} \frac{\partial^2 Z_{i,n_{ij}}}{\partial R_{s,1} \partial I_{s,k}} & \dots & \dots \end{pmatrix}$$

$$\mathbf{B}_i^Z = \begin{pmatrix} \frac{\partial Z_{i,1}}{\partial R_{i,1}} + \sum_{k=1}^{nI_i} \frac{\partial^2 Z_{i,1}}{\partial R_{i,1} \partial I_{i,k}} & \dots & \frac{\partial Z_{i,1}}{\partial R_{i,nR_i}} + \sum_{k=1}^{nI_i} \frac{\partial^2 Z_{i,1}}{\partial R_{i,nR_i} \partial I_{i,k}} \\ \dots & \dots & \dots \\ \frac{\partial Z_{i,n_{ij}}}{\partial R_{i,1}} + \sum_{k=1}^{nI_i} \frac{\partial^2 Z_{i,n_{ij}}}{\partial R_{i,1} \partial I_{i,k}} & \dots & \frac{\partial Z_{i,n_{ij}}}{\partial R_{i,nR_i}} + \sum_{k=1}^{nI_i} \frac{\partial^2 Z_{i,n_{ij}}}{\partial R_{i,nR_i} \partial I_{i,k}} \end{pmatrix}$$

$$\frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{ki}} = \begin{pmatrix} \frac{\partial Z_{i,1}}{\partial Y_{ki,1}} & \frac{\partial Z_{i,1}}{\partial Y_{ki,2}} & \dots & \frac{\partial Z_{i,1}}{\partial Y_{ki,n_{ki}}} \\ \frac{\partial Z_{i,2}}{\partial Y_{ki,1}} & \frac{\partial Z_{i,2}}{\partial Y_{ki,2}} & \dots & \frac{\partial Z_{i,2}}{\partial Y_{ki,n_{ki}}} \\ \dots & \dots & \dots & \dots \\ \frac{\partial Z_{i,n_{ij}}}{\partial Y_{ki,1}} & \frac{\partial Z_{i,n_{ij}}}{\partial Y_{ki,2}} & \dots & \frac{\partial Z_{i,n_{ij}}}{\partial Y_{ki,n_{ki}}} \end{pmatrix}$$

$$\frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_i} = \left( \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{1i}}, \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{2i}}, \dots, \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{(i-1)i}}, \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{(i+1)i}}, \dots, \frac{\partial \mathbf{Z}_i}{\partial \mathbf{Y}_{nS}} \right)$$

# Robustness Assessment

- Step 3: calculate  $\sigma_Z^{\min}$  and  $\sigma_Z^{\max}$

$$\sigma_Z^2 = \mathbf{Q}(\mathbf{I})\sigma_{R_S}^2 + \mathbf{T}(\mathbf{I})\sigma_R^2$$

$\mathbf{Q}(\mathbf{I}), \mathbf{T}(\mathbf{I})$ : functions of  $\mathbf{I}$ ,

including 1st and 2nd derivatives

$$\min_{\mathbf{I}} \sigma_Z(\mathbf{I})$$

$$s.t. \mathbf{I}^l \leq \mathbf{I} \leq \mathbf{I}^u$$

# Example 1: 4-Bar Linkage

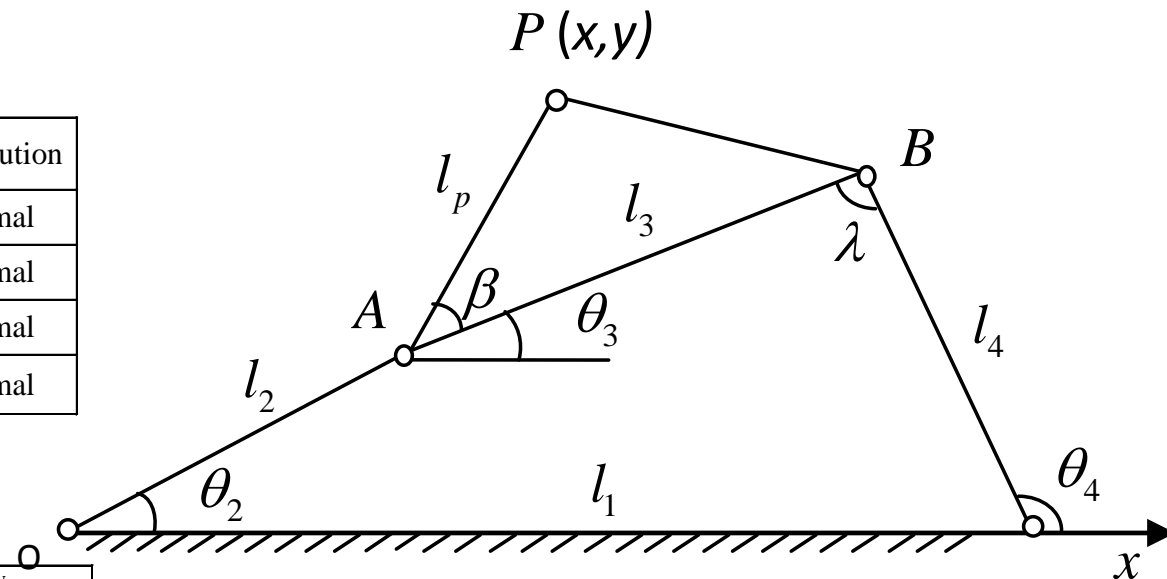
## Single Discipline

Random variables

Variable	Mean	Standard Deviation	Distribution
$R_1(l_2)$	51.68mm	0.20 mm	Normal
$R_2(l_3)$	297.06mm	0.20 mm	Normal
$R_3(l_4)$	197.08mm	0.20 mm	Normal
$R_4(l_p)$	99.11mm	0.20 mm	Normal

Interval variables

Variable	$I^L$	$I^U$
$I_1(l_1)$	$\bar{l}_1 - 0.5 \text{ mm}$	$\bar{l}_1 + 0.5 \text{ mm}$
$I_2(\beta)$	$\bar{\beta} - 1^\circ$	$\bar{\beta} + 1^\circ$



Output:  $P(x,y)$

# 4-Bar Linkage - Results

	GRA	MCS
at 10°	(0.178,0.203) mm	(0.172,0.207) mm
at 10°	(0.177 ,0.203) mm	(0.171,0.207) mm
at 60°	(0.149,0.260) mm	(0.148,0.261) mm
at 60°	(0.148 ,0.259) mm	(0.146 ,0.259) mm

GRA: General robustness assessment



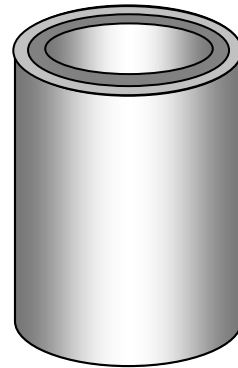
# Multidisciplinary Cylinder Problem

Output:  $P(x,y)$

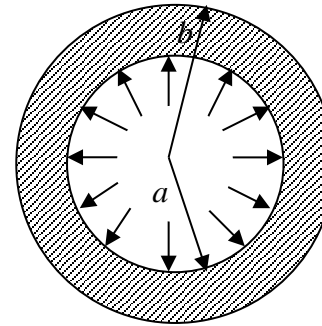
$$Z_1^{(1)} = \sigma_a - S$$

$$Z_1^{(2)} = \sigma_b - S$$

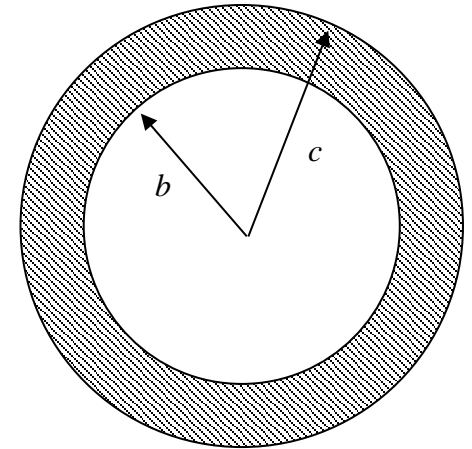
$\sigma_a$  and  $\sigma_b$ : stresses  
at a and b  
S: strength



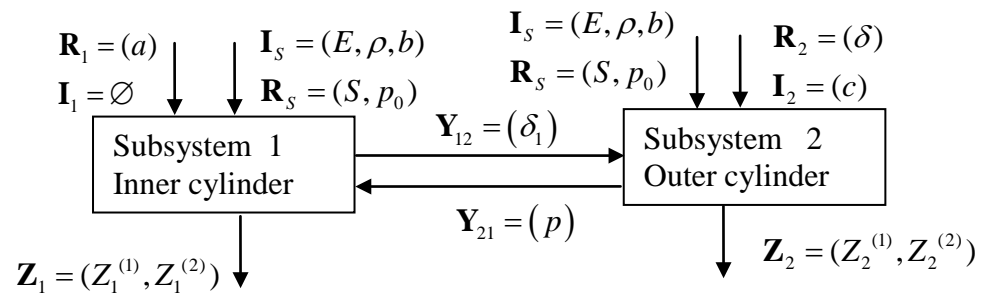
Compound cylinder system



Subsystem 1: Inner cylinder



Subsystem 2: Outer cylinder



# Cylinder Problem

## Random variables

Variables	Mean	Standard Deviation	Distribution
$S$	$10.0 \times 10^3$ psi	$1.0 \times 10^3$ psi	Normal
$p_0$	$20.0 \times 10^3$ psi	$2.0 \times 10^3$ psi	Normal
$a$	75 in	0.1 in	Normal
$\delta$	0.004 in	0.0004 in	Normal

## Interval variables

Variables	$I^L$	$I^U$
$E$	$30 \times 10^6 \times (1 - 2\%)$ psi	$30 \times 10^6 \times (1 + 2\%)$ psi
$\rho$	$0.3 \times (1 - 2\%)$	$0.3 \times (1 + 2\%)$
$b$	9.95 in	10.05 in
$c$	14.95 in	15.05 in

## Result

	GRA	MCS
$\sigma_{z_1}^{\max}$ (psi)	$[3.485 \times 10^3 \ 2.444 \times 10^3]$	$[3.597 \times 10^3 \ 2.570 \times 10^3]$
$\sigma_{z_1}^{\min}$ (psi)	$[3.484 \times 10^3 \ 2.419 \times 10^3]$	$[3.562 \times 10^3 \ 2.515 \times 10^3]$
$\sigma_{z_2}^{\max}$ (psi)	$[2.40 \times 10^3 \ 1.667 \times 10^3]$	$[2.544 \times 10^3 \ 1.750 \times 10^3]$
$\sigma_{z_2}^{\min}$ (psi)	$[2.373 \times 10^3 \ 1.667 \times 10^3]$	$[2.50 \times 10^3 \ 1.724 \times 10^3]$

# Conclusions

- The robustness assessment is efficient.
- The accuracy is good when standard deviations and widths are small.
- The method is not applicable when the performance function is expanded at a saddlepoint.
- Future work will be the use of the method for robust design.

# Acknowledgement

- NSF CMMI 0400081.
- China Scholarship Council.