

1-4. The allowable average shear stress  $\tau_b$  in each of the 5-mm diameter bolts follows a normal distribution,  $\tau_{ab} \sim N(75, 6^2)$  MPa . Along the four shaded shear planes the allowable average shear stress also follows a normal distribution,  $\tau_{ap} \sim N(0.35, 0.03^2)$  MPa . Determine the maximum axial force  $P$  that can be applied to the joint, as shown in Fig. 1.4.1, if the probabilities of failure of the bolts and shear planes of the member are less than  $10^{-4}$  .

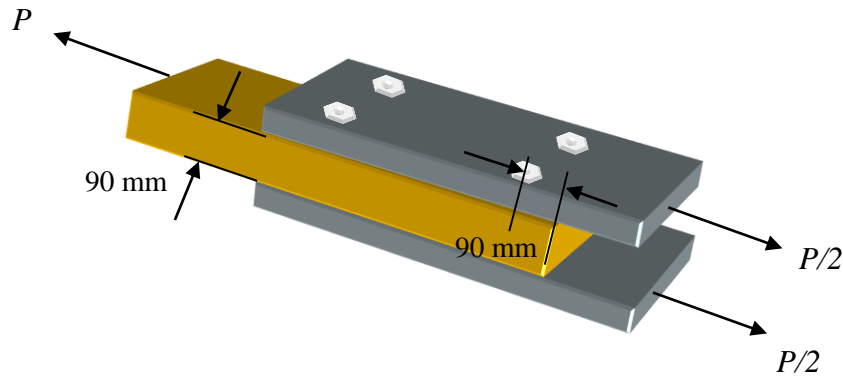


Fig. 1.4.1

### Solution

**Internal loading:** The shear force developed on each shear plane of the bolt and the member can be determined by solving the force equation of equilibrium according to the free-body diagrams as shown in Figs. 1.4.2 and 1.4.3, respectively.

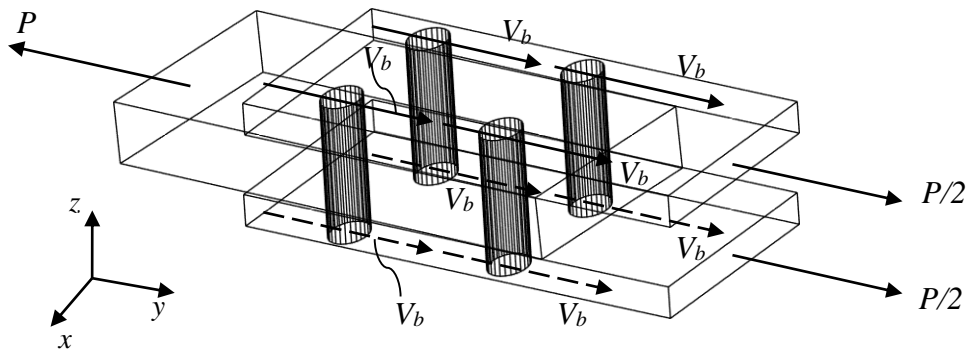


Fig. 1.4.2

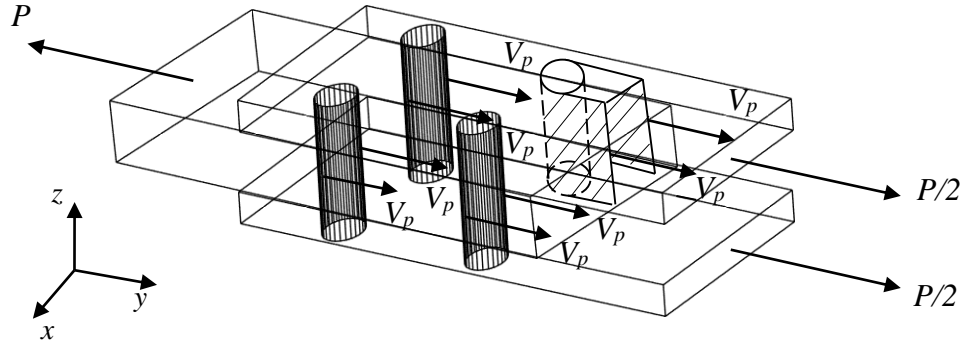


Fig. 1.4.3

$$\begin{aligned} \Sigma F_y = 0; \quad 4V_b - P = 0; \quad V_b &= P/4 \\ \Sigma F_y = 0; \quad 4V_p - P = 0; \quad V_p &= P/4 \end{aligned}$$

**Average Shear Stress:** The areas of each shear plane of the bolts and the members are

$$A_b = \frac{\pi}{4} (0.005^2) = 19.625 \times 10^{-6} \text{ m}^2 \quad \text{and} \quad A_p = 0.09^2 = 0.0081 \text{ m}^2, \text{ respectively.}$$

We obtain

$$\tau_b = \frac{V_b}{A_b} = \frac{P/4}{19.625 \times 10^{-6}} = 1.27 \times 10^4 P; \quad \tau_p = \frac{V_p}{A_p} = \frac{P/4}{0.0081} = 30.864 P$$

Let  $Y_b = \tau_b - \tau_{ab}$ , the probability of failure of each bolt can be expressed as

$$p_f = \Pr(Y_b = \tau_b - \tau_{ab} > 0) < 10^{-4}.$$

We can get  $\mu_{Y_b}$  and  $\sigma_{Y_b}$  using

$$\mu_{Y_b} = \tau_b - \mu_{\tau_{ab}} = 1.27 \times 10^4 P - 75 \times 10^6; \quad \sigma_{Y_b} = \sigma_{\tau_{ab}} = 6 \times 10^6$$

Then

$$p_f = \Pr(Y_b > 0) = \Pr\left(\frac{Y_b - \mu_{Y_b}}{\sigma_{Y_b}} > \frac{-\mu_{Y_b}}{\sigma_{Y_b}}\right) = 1 - \Phi\left(\frac{-\mu_{Y_b}}{\sigma_{Y_b}}\right) = 1 - \Phi\left(\frac{-(1.27 \times 10^4 P - 75 \times 10^6)}{6 \times 10^6}\right) < 10^{-4}$$

We can obtain that  $P < 662 \text{ N}$  (controls).

**Ans.**

Let  $Y_p = \tau_p - \tau_{ap}$ , the probability of failure of shear planes can be expressed as

$$p_f = \Pr(Y_p = \tau_p - \tau_{ap} > 0) < 10^{-4}.$$

We can get  $\mu_{Y_p}$  and  $\sigma_{Y_p}$  using

$$\mu_{Y_p} = \tau_p - \mu_{\tau_{ap}} = 30.864P - 0.35 \times 10^6; \quad \sigma_{Y_p} = \sigma_{\tau_{ap}} = 0.03 \times 10^6$$

Then

$$p_f = \Pr(Y_b > 0) = \Pr\left(\frac{Y_p - \mu_{Y_p}}{\sigma_{Y_p}} > \frac{-\mu_{Y_p}}{\sigma_{Y_p}}\right) = 1 - \Phi\left(\frac{-\mu_{Y_p}}{\sigma_{Y_p}}\right) = 1 - \Phi\left(\frac{-(30.864P - 0.35 \times 10^6)}{0.03 \times 10^6}\right) < 10^{-4}$$

We can obtain  $P < 7725\text{N}$ .